positions on finite regions of the frequency axis. This "zero-moving" method produces a good (i.e., effective) approximation to a low-pass brick wall amplitude function (FIGURE 8f). Similar methods exist for band-pass and high-pass infinite slope crossover filters. These methods are described in detail in the inventor's '466 patent.--

Kindly amend the paragraph beginning on page 10, line 24 as indicated.

--Respectively shown at 144 and 144' in FIGURES 8c and 8f are slopes in the amplitude response of the low-pass filters in each respective FIGURE 8a and 8d. In FIGURE 8c, the slope 144 in response, resulting from the 3-element low-pass filter (FIGURE 8a), is 18dB/octave. In FIGURE 8f, the slope 144' ~~is on the order of~~ may be as high as 120dB/octave in the very best embodiments of the invention, which is generally recognized by those skilled in the art as a good or useful approximation to the brick wall amplitude function.--

Kindly replace Equation 7 on page 11 with:

$$M = \frac{(L11 - L22)}{4}$$

Kindly amend the paragraph beginning on page ~~10~~ 12, line ~~24~~ 19 as indicated.

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--This gives M a value of 0.15 millihenry from Equation (7), making K equal to 0.15 from Equation (6). This transformer 152 is incorporated into the loudspeaker system crossover of FIGURE 10. Amplitude response 154 (FIGURE 11) of a midrange driver has slope 156 ~~on the order of 100dB/octave in accordance with the present invention~~ of at least 40 dB/octave and, in better embodiments of the present invention, up to 120 db/octave.--